

AD A 136156

TECHNICAL LIBRARY

	F
AD	

TECHNICAL REPORT ARLCB-TR-83038

ELASTIC PROPERTIES OF URANIUM - .78 TITANIUM AS A FUNCTION OF PRESSURE TO 1.6 GPa

J. FRANKEL
D. DANDEKAR

OCTOBER 1983



US ARMY ARMAMENT RESEARCH AND DEVELOPMENT CENTER LARGE CALIBER WEAPON SYSTEMS LABORATORY BENÉT WEAPONS LABORATORY WATERVLIET N.Y. 12189

APPROVED FOR PUBLIC RELEASE; DISTRIBUTION UNLIMITED

DISCLAIMER

The findings in this report are not to be construed as an official Department of the Army position unless so designated by other authorized documents.

The use of trade name(s) and/or manufacture(s) does not constitute an official indorsement or approval.

DISPOSITION

Destroy this report when it is no longer needed. Do not return it to the originator.

REPORT DOCUMENTATION PAGE	READ INSTRUCTIONS BEFORE COMPLETING FORM
1. REPORT NUMBER 2. GOVT ACCESSION NO ARLCB-TR-83038	. 3. RECIPIENT'S CATALOG NUMBER
ARBESTIC PROPERTIES OF URANIUM78 TITANIUM AS A FUNCTION OF PRESSURE TO 1.6 GPa	s. Type of Report & Period Covered Final
	5. PERFORMING ORG. REPORT NUMBER
7. AUTHOR(*) J. Frankel and D. Dandekar* *See Reverse	8. CONTRACT OR GRANT NUMBER(e)
9. PERFORMING ORGANIZATION NAME AND ADDRESS US Army Armament Research & Development Center Benet Weapons Laboratory, DRSMC-LCB-TL Watervliet, NY 12189	10. PROGRAM ELEMENT, PROJECT, TASK AREA & WORK UNIT NUMBERS AMCMS No. 611102H600011 PRON No. 1A1283121A1A
US Army Armament Research & Development Center Large Caliber Weapon Systems Laboratory Dover, NJ 07801	12. REPORT DATE October 1983 13. NUMBER OF PAGES 10
14. MONITORING AGENCY NAME & ADDRESS(II different from Controlling Office)	1S. SECURITY CLASS. (of this report) UNCLASSIFIED 1S. DECLASSIFICATION/DOWNGRADING SCHEDULE

16. DISTRIBUTION STATEMENT (of thie Report)

Approved for public release; distribution unlimited.

17. DISTRIBUTION STATEMENT (of the abetract entered in Block 20, if different from Report)

18. SUPPLEMENTARY NOTES

Presented at AIRAPT Conference, Uppsala, Sweden, 15-22 August 1981. Published in proceedings of the conference.

19. KEY WORDS (Continue on reverse side if necessary and identify by block number)

Uranium

Ultrasonic Velocities

Pressure

Elastic Properties

20. ABSTRACT (Continue on reverse side if necessary and identify by block number)

The transit time for passage of longitudinal and shear ultrasonic waves through polycrystalline depleted uranium - .78 weight percent titanium (Ti) alloy was determined as a function of pressure in a hydrostatic medium. Specimens of two thicknesses were used in order to eliminate bond-transducer effects from transit time determinations. The longitudinal velocity v_L increases 3.5 percent from one atmosphere to a value of 3.48 km/sec at 1.6 GPa; the shear (CONT'D ON REVERSE)

DD 1 JAN 73 1473

EDITION OF 1 NOV 65 IS OBSOLETE

UNCLASSIFIED

•	AUTHORS										
	D. Dandeka U.S. Army		lals an	d Mecha	ınics l	Research	Cente	er			
	Watertown						2				
0.	ABSTRACT										
ner	city v _s in eases 8.1 ent to 81	percei	nt to a	value	of 120) GPa an	d the	adiabat shear n	ic bul odulus	k modulus μ, 9.4	B BS
	circ to or	014 0	TOL DIE	ounc p	,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,	.c zango	•				

TABLE OF CONTENTS

	Page
INTRODUCTION	1
EXPERIMENTAL DETAILS	1
DATA ANALYSIS	3
REFERENCES	5
TABLES	
I. VALUE OF COEFFICIENTS FROM STRAIGHT LINE FIT $1/\Delta fm = a_OP + a$ TO DATA	1 6
II. ESTIMATE OF PRESSURE DEPENDENCE OF TRANSIT TIMES FOR LONGITUDINAL AND SHEAR WAVES IN DU78 Ti OF INITIAL THICKNESS 4.863 MM	7
III. ELASTIC PROPERTIES	7
LIST OF ILLUSTRATIONS	
1. Schematic of Measurement.	8
2. 1/Δfm Against Pressure.	9

INTRODUCTION

Ultrasonic measurements to a pressure of 1.8 GPa in pure depleted uranium (DU) by a pulse overlap technique were previously reported by Abey and Bonner (ref 1). The present measurements with a different technique show that within experimental errors the present alloying does not markedly change the elastic properties of the material in the pressure range studied.

EXPERIMENTAL DETAILS

DU alloyed with .78 weight percent titanium was obtained from the Oak Ridge National Laboratory. An ingot cast of U - .78% Ti was first forged and rolled at 913° K in vacuum and water quenched, then aged at 643° K in an argon atmosphere, and water cooled. The quench brought the uranium from the $\gamma(bcc)$ phase to the α (orthorhombic) phase and the aging treatment served to reduce voids and residual stresses. The microstructure of the material was acicular. Observation of the microstructure and shear velocity measurements with varying shear wave polarizations suggest that the acicular grains had a very mild anisotropy in one direction. Measurements were made in the specimen direction which showed no anisotropy.

The starting material was fabricated into two cubes whose opposing faces were parallel to .0003 cm over each face. Special care was taken for an even thin bond. The bonding material was a rapid room temperature curing cyanoacrylate MIL-A-460508 type 1 class 2 by Loctite. The resonance frequency of the Lithium Niobate transducers was 10 or 15 MHz. This was considerably

¹Abey, A. E. and Bonner, B. P., Jour. Appl. Phys., <u>1975</u>, Vol. 46, No. 4, 1427-1428.

reduced by bonding and mildly increased by pressure. Pressure was applied in a Birch-Bridgman 30 Kbar system with a 50-50 Pentane-Isopentane mixture as a pressure medium.

The measurement method is based on the use of the double balanced mixer, and is described by Peterson et al (ref 2) (Fig. 1). When two coherent waves are combined in the mixer with proper amplitudes, the mixer output is zero volts (a null echo) if they have a 90 degree phase relationship. This is equivalent to saying that there is an integer $n \pm 1/4$ number of rf periods in the continuous wave (CW) during the time interval in which it takes the ultrasonic wave to produce the mth echo at the transducer.

The measurement involves finding two frequencies. First a frequency is found for a null echo, then for another null, m (where m= echo number) extra periods are included in the time interval T_m by increasing the frequency to f'.

$$T_{m} = \frac{n \pm 1/4}{f} = \frac{n + m \pm 1/4}{f'} = mT_{rt}$$
 (1)

The uncorrected round-trip time in the specimen is

$$T_{rt} = \frac{1}{f' - f} = \frac{1}{\Delta f_m}$$
 (2)

The time $T_{\rm m}$ in reality is given by ${\rm mT_{rt}}$ less any delays. These are caused by the electronics and any phase changes at the transducer-specimen interface. One could make estimates of these corrections with available approximate theories by making measurements for two or more echoes. These require

Peterson, G. L., Chick, B., and Junker, W., 1975 Ultr. Symp Proc., 650-653, IEE Cat. No. CHO 994-4SU.

measurements at exactly the resonance frequency of the transducer, equal confidence in measurements on different echoes, and knowledge (not available for lithium niobate) of the transducer acoustic impedance for the pressures of the experiment.

We found the most useful approach was to avoid estimates of the above effects and to evaluate the transit times by a difference method: We measured the Δfm in a given specimen for two echoes m=2 and m=3. The specimen was then reduced in thickness and the Δfm was found with the same transducer and bond. The difference of the inverse Δfm for the two specimen thicknesses gave the travel time for the thickness of the residual specimen (.4683 cm at P=1 atm.). Data on a second specimen of equal thickness with the first was also used and its values fell within the scatter of the first. Frequencies of measurement were reproduced at equivalent pressures for the thick and thin specimens (Figure 2).

DATA ANALYSIS

Data were separated according to echo number (m = 2 or 3) thick or thin specimen and longitudinal or shear wave. A straight line fit of the form $1/\Delta fm = a_0P+a_1$, was made through all data of each type by the method of least squares. Units of P are in GPa and $1/\Delta fm$ in μ sec and r is the regression coefficient (Table I). The linear fit is justified by the high correlation coefficients and by the small changes in transit times obtained. The transit times in the residual portion of the specimen were obtained by subtraction (Table II). On the basis of the regression fit and averaging of the m = 2 and m = 3 data, the standard deviations for transit times of the longitudinal and

shear waves are respectively $\sigma_L = .018$ and $\sigma_S = .031$.

An iteration process developed by Dandekar (ref 3) was used in determining the specimen length and ultimately the velocities from the transit times. Variations in $1+\Delta=B^S/B^T$ are included. Here

$$\Delta(P) = \beta^{2}(P) B^{S}(p) T/\rho(P) C_{p}(P)$$
 (3)

where β is the volume expansion coefficient and C_p is the specific heat. References 4 and 5 were used to obtain the thermodynamic data for estimating $\Delta(P)$. Because of the small changes involved, the iteration is only performed at 1.6 GPa; so we only report velocities and bulk moduli at that pressure (Table III). From the slopes of the bulk and shear moduli, we also get $dB^s/dP = 5.5$ and $d\mu/dP = 4.4$

Within the error of the experiment which is larger for the pressure derivatives, these values correlate with those reported by Abey and Bonner (ref 1).

¹Abey, A. E. and Bonner, B. P., Jour. Appl. Phys., 1975, Vol. 46, No. 4, 1427-1428.

³Dandekar, C., Jour. Appl. Phys., 1970, Vol. 41, No. 2, 667-672.

⁴AIP Handbook, Coord. Ed., D. E. Gray, Third Edition, 1972, McGraw-Hill, NY. ⁵Fisher, E. S., J. Nucl. Mat. 1966, 18, 39.

REFERENCES

- Abey, A. E. and Bonner, B. P., Jour. Appl. Phys., 1975, Vol. 46, No. 4, 1427-1428.
- Peterson, G. L., Chick, B., and Junker, W., 1975 Ultr. Symp Proc., 650-653, IEEE Cat No. CHO 994-4SU.
- 3. Dandekar, D., Jour. Appl. Phys., 1970, Vol. 41, No. 2, 667-672.
- 4. AIP Handbook, Coord. Ed., D. E. Gray, Third Edition, 1972, McGraw-Hill, NY.
- 5. Fisher, E. S., J. Nucl. Mat. 1966, 18, 39.

TABLE I. VALUE OF COEFFICIENTS FROM STRAIGHT LINE FIT $1/\Delta fm = a_OP \, + \, a_1 \, \, TO \, \, DATA$

						1								
Spec		Thi	Thick			Thin	d.			Resid	ual Leng	Residual Length = 4.863 mm	.3 mm	
Echo	m = 3	د	E	n = 2	# #	3	m = 2	2	E = 3	3	m = 2	2	<ave></ave>	e>
Wave	Shear	Long	Shear	Long	Shear	Long	Shear	Long	Shear	Long	Shear	Long	Shear	Long
a _o	12.906	7.734	12.935	7.758	8.029	4.839	8.053	4.856	4.876	2.895	4.883	2.902	4.879	2.897
-a1	.235	.168	. 222	.175	.0865	.101	6660.	.102	.1485	.0688	.1217	.0727	.135	.07135
ı.	.9423	.9730	.9807	.9813	.9510	.9718	.9715	.9726	.0535	.0258	.0324	.0324	ı	1
							T		+					

TABLE II. ESTIMATE OF PRESSURE DEPENDENCE OF TRANSIT TIMES FOR LONGITUDINAL AND SHEAR WAVES IN DU - .78 Ti OF INITIAL THICKNESS 4.863 MM

Pressure (GPa)	Transit 1	ľime (μs)
+:	Long.	Shear
0.0 0.4 0.8 1.2 1.6	1.449 1.434 1.419 1.406 1.342	2.439 2.413 2.386 2.358 2.331

TABLE III. ELASTIC PROPERTIES

	P = 0	P = 1.6 GPa
VL	3.36 ± .04 km/sec	3.48
Vs	1.99 ± .03 km/sec	2.08
B ^S	111 ± 5 GPa	120
μ	74 ± 2 GPa	81
BT	108 ± 5 GPa	117

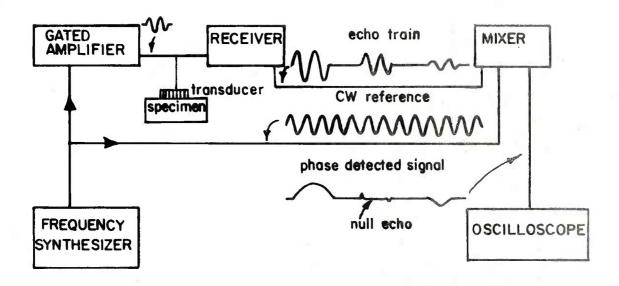


Figure 1. Schematic of Measurement.

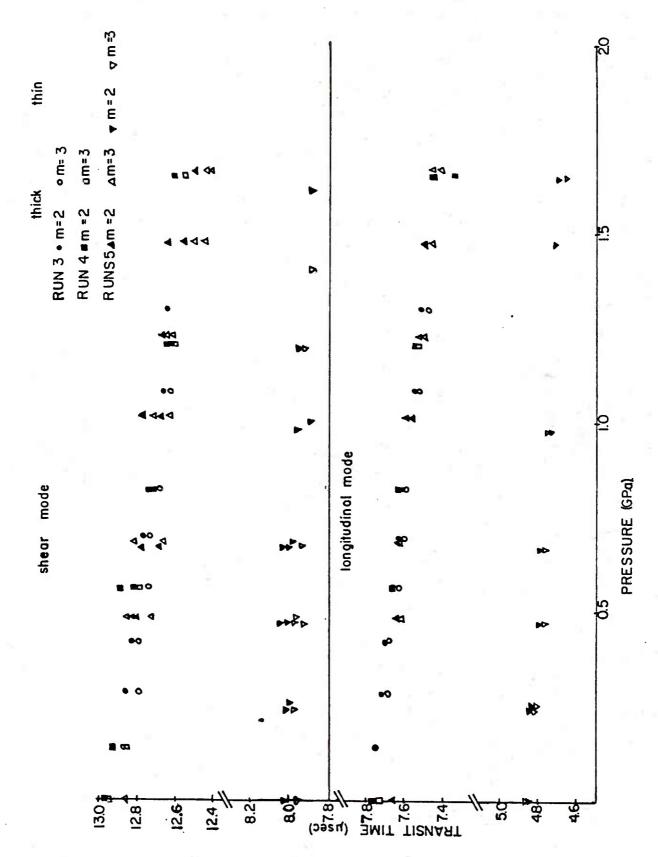


Figure 2. $1/\Delta fm$ Against Pressure.

READER EVALUATION

Please take a few minutes to complete the questionnaire below and return to us at the following address: Commander, Armament Research and Development Center, U.S. Army AMCCOM, ATTN: Technical Publications, DRSMC-LCB-TL, Watervliet, NY 12189.

1.	Benet Weapons Lab. Report Number
2.	Please evaluate this publication (check off one or more as applicable). Yes No
	Information Relevant
	Information Technically Satisfactory
	Format Easy to Use
	Overall, Useful to My Work
	Other Comments
3.	Has the report helped you in your own areas of interest? (i.e. preventing
	duplication of effort in the same or related fields, savings of time, or
	money).
4.	How is the report being used? (Source of ideas for new or improved
	designs. Latest information on current state of the art, etc.).
_	
5.	How do you think this type of report could be changed or revised to
	improve readability, usability?
6.	Would you like to communicate directly with the author of the report
	regarding subject matter or topics not covered in the report? If so
	please fill in the following information.
	Name:
	Telephone Number:
	Organization Address:

TECHNICAL REPORT INTERNAL DISTRIBUTION LIST

			COPIES
	OPMEN'T ENGINEERING BRANCH DRSMC-LCB-D -DP -DR		1 1 1
	-DS (SYSTEMS) -DS (ICAS GROUP) -DC		1 1 1
	IEERING SUPPORT BRANCH DRSMC-LCB-S -SE	i de la companya de	1 1
CHIEF, RESEA	ARCH BRANCH DRSMC-LCB-R -R (ELLEN FOGARTY) -RA -RM -RP -RT		2 1 1 1 1 1
TECHNICAL LI ATTN:	IBRARY DRSMC-LCB-TL		5
	JBLICATIONS & EDITING UNIT DRSMC-LCB-TL		2
DIRECTOR, OF	PERATIONS DIRECTORATE		1
DIRECTOR, PR	ROCUREMENT DIRECTORATE		1
DIRECTOR, PE	RODUCT ASSURANCE DIRECTORATE		1

NOTE: PLEASE NOTIFY DIRECTOR, BENET WEAPONS LABORATORY, ATTN: DRSMC-LCB-TL, OF ANY ADDRESS CHANGES.

TECHNICAL REPORT EXTERNAL DISTRIBUTION LIST

	NO. OF		O. CF
ASST SEC OF THE ARMY RESEARCH & DEVELOPMENT ATTN: DEP FOR SCI & TECH	1		1
THE PENTAGON WASHINGTON, D.C. 20315		ROCK ISLAND, IL 61299 COMMANDER	
COMMANDER DEFENSE TECHNICAL INFO CENTER ATTN: DTIC-DDA CAMERON STATION	12	ROCK ISLAND ARSENAL ATTN: SMCRI-ENM (MAT SCI DIV) ROCK ISLAND, IL 61299	1
ALEXANDRIA, VA 22314 COMMANDER		DIRECTOR US ARMY INDUSTRIAL BASE ENG ACTV ATTN: DRXIB-M	1
US ARMY MAT DEV & READ COMD ATTN: DRCDE-SG	1	ROCK ISLAND, IL 61299	
5001 EISENHOWER AVE ALEXANDRIA, VA 22333		COMMANDER US ARMY TANK-AUTMV R&D COMD ATTN: TECH LIB - DRSTA-TSL	1
COMMANDER ARMAMENT RES & DEV CTR US ARMY AMCCOM		WARREN, MI 48090 COMMANDER	
ATTN: DRSMC-LC(D) DRSMC-LCE(D) DRSMC-LCM(D) (BLDG 321)	1 1 1	US ARMY TANK-AUTMV COMD ATTN: DRSTA-RC WARREN, MI 48090	1
DRSMC-LCS(D) DRSMC-LCU(D) DRSMC-LCW(D)	1 1 1	COMMANDER US MILITARY ACADEMY	
DRSMC-SCM-O (PLASTICS TECH EVAL CTR, BLDG. 351N)		ATTN: CHMN, MECH ENGR DEPT WEST POINT, NY 10996	1
DRSMC-TSS(D) (STINFO) DOVER, NJ 07801 DIRECTOR	2	US ARMY MISSILE COMD REDSTONE SCIENTIFIC INFO CTR ATTN: DOCUMENTS SECT, BLDG. 4484 REDSTONE ARSENAL, AL 35898	2
BALLISTICS RESEARCH LABORATORY ARMAMENT RESEARCH & DEV CTR US ARMY AMCCOM	1	COMMANDER US ARMY FGN SCIENCE & TECH CTR	
ATTN: DRSMC-TSB-S (STINFO) ABERDEEN PROVING GROUND, MD 21005		ATTN: DRXST-SD 220 7TH STREET, N.E. CHARLOTTESVILLE, VA 22901	1
MATERIEL SYSTEMS ANALYSIS ACTV ATTN: DRSXY-MP ABERDEEN PROVING GROUND, MD 21005	1		

NOTE: PLEASE NOTIFY COMMANDER, ARMAMENT RESEARCH AND DEVELOPMENT CENTER, US ARMY AMCCOM, ATTN: BENET WEAPONS LABORATORY, DRSMC-LCB-TL, WATERVLIET, NY 12189, OF ANY ADDRESS CHANGES.

TECHNICAL REPORT EXTERNAL DISTRIBUTION LIST (CONT'D)

	NO. OF COPIES		NO. OF COPIES	
COMMANDER US ARMY MATERIALS & MECHANICS RESEARCH CENTER ATTN: TECH LIB - DRXMR-PL WATERTOWN, MA 01272	2	DIRECTOR US NAVAL RESEARCH LAB ATTN: DIR, MECH DIV CODE 26-27, (DOC LIB) WASHINGTON, D.C. 20375	1 1	
COMMANDER US ARMY RESEARCH OFFICE ATTN: CHIEF, IPO P.O. BOX 12211 RESEARCH TRIANGLE PARK, NC 27709	1	COMMANDER AIR FORCE ARMAMENT LABORATORY ATTN: AFATL/DLJ AFATL/DLJG EGLIN AFB, FL 32542	1 1	
COMMANDER US ARMY HARRY DIAMOND LAB ATTN: TECH LIB 2800 POWDER MILL ROAD ADELPHIA, MD 20783	1	METALS & CERAMICS INFO CTR BATTELLE COLUMBUS LAB 505 KING AVENUE COLUMBUS, OH 43201	1	
COMMANDER NAVAL SURFACE WEAPONS CTR ATTN: TECHNICAL LIBRARY CODE X212 DAHLGREN, VA 22448	Ī			

NOTE: PLEASE NOTIFY COMMANDER, ARMAMENT RESEARCH AND DEVELOPMENT CENTER, US ARMY AMCCOM, ATTN: BENET WEAPONS LABORATORY, DRSMC-LCB-TL, WATERVLIET, NY 12189, OF ANY ADDRESS CHANGES.